

European Commission

# **Physics-augmented models to simulate commercial adaptive** cruise control (ACC) systems

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# Introduction

Accurate simulation of mixed traffic, including human-driven vehicles (HDVs) and automated vehicles (AVs), is crucial to the development and assessment of cooperative, connected, and automated mobility (CCAM) technologies. To reproduce driving behaviors of HDVs and AVs, car-following (CF) and adaptive cruise control (ACC) models are developed in the literature of traffic flow. Moreover, these models are augmented to capture essential but overlooked aspects, e.g., vehicle dynamics, perception/actuation delays, and acceleration capabilities. However, a systematic analysis of models augmented with those aspects at different levels of detail is still lacking. This study, therefore, compares the accuracy and robustness of 90 different models, resulting from all possible combinations of five base CF/ACC models and different physics extensions, including vehicle dynamics, acceleration constraints, and perception delay.



2) Gipps' model:

 $\begin{cases} a_{n,cmd}(t) = \min\left[k_v \cdot \Delta v_n(t) + k_s \cdot \Delta s_n(t), k_0 \cdot \left(v_0 - v_n(t)\right)\right], \\ \Delta s_n(t) = s_n(t) - s_{n,des}(t), \end{cases}$ 

Constant time headway  
(CTH) spacing policy:  

$$s_{n,des}(t) = s_0 + t_h \cdot v_n(t),$$
(7)
pps-equilibrium  
spacing policy:  

$$s_{n,des}(t) = s_0 + (t_h + \theta)v_n(t) - 0.5v_n(t)^2 \left(\frac{1}{a_{min}} - \frac{1}{\hat{a}_{min}}\right),$$
(8)

### **II. Physics extensions**

**U** Vehicle dynamics (VD)

 $a_{n,0}(t) =$ 1) None:

$$a_{n,cmd}(t),$$

(6)

(9)

(10)

(13)

 $\tau_a \cdot \dot{a}_{n,0}(t) + a_{n,0}(t) = a_{n,cmd}(t),$ 2) Linear (LVD):

F(t) - F(t)

Preceding vehicle (n-1)

Following vehicle (*n*)

#### **Fig. 1.** Kinematics in car-following problems.

The movement of the following vehicle (n) depends not only on the trajectory of the preceding vehicle (n-1), but also on the characteristics of the follower vehicle, driver/ACC, road, etc. In car-following problems, main variables include acceleration (a), speed (v), position (x), and inter-vehicle spacing (s).

# Modelling framework



3) Nonlinear	$a_{n,0}(t) = \frac{T_t(t) - T_r(t)}{\phi \cdot m},$
(NLVD):	$\int F_r(t) = f_0 \cdot \cos \alpha(t) + f_1 \cdot v_n(t) + f_2 \cdot v_n(t)^2 + mg \cdot \sin \alpha(t), $ (11)
	$\int F_t(t) = \frac{T_t(t)}{r_w} = m \cdot a_t(t), \tag{11}$
	$ \tau_a \cdot \dot{a}_t(t) + a_t(t) = a_{n,cmd}(t), $
Acceleration c	constraints (AC)

- $a_n(t) = a_{n,0}(t),$ (12)1) None:
- $a_n(t) = \max\{a_{lb}, \min[a_{n,0}(t), a_{ub}]\},\$ 2) Constant:
- 3) Microsimulation free-flow acceleration (MFC) boundary model:

$$a_n(t) = \max\left\{a_{dp}(v_n(t)), \min\left[a_{n,0}(t), a_{ap}(v_n(t))\right]\right\},\tag{14}$$

- Perception delay (PD)
- $\tau_p = 0,$ (15)1) None:
- $\tau_p > 0,$ (16)2) Constant:

### III. Summary of 90 models

																	_			
Model	Mod	el ACO	С	Spacing			Perception	l	Vehicle	A	Acceleration	Ca	libration							
groups	ID	cont	troller		pol	icy			delay (PD)	)	dynamic	cs (VD) C	Constraints (AC)	pa	rameters					
S	73	Line	ear cont	tr., Eq. (6)	Gip	ps-equilib	rium, Eq	. (8)	None, Eq.	(15)	None, E	q. (9) N	lone, Eq. (12)	$k_{s}$	$k_v, k_0, v_0, s_0, t_h,$	$ heta$ , $a_{min}$ , $\hat{a}_{min}$				
del	74	Model	Mode	el AC	0		Spaci	ng		Perc	ception	Vehicle	Acce	eleration	Calibr	ation				
om	75	groups	ID	cont	roller		policy	/		dela	ay (PD)	dynamics	(VD) Cons	straints (AC	C) parame	eters				
sed	76	76 55		Line	ear contr.	, Eq. (6)	IDM-	DM-desired, Eq. (3)		Nor	ne, Eq. (15)	None, Eq.	(9) None	e, Eq. (12)	$k_s, k_v,$	$k_0, v_0, s_0, t_h, a_{max}$ , a	min			
-ba	77	ləbd	56	Model	Mode	l ACC	1		Spacing	5		Perception	Vehicle		Acceleration	Calibrati	on			
sdc	78	mc	57	groups	ID	contr	oller		policy			delay (PD)	dynamics	(VD)	Constraints (A	C) paramete	ers			
-Gij	79	sed	58	s	37	Line	ar contr.,	Eq. (6)	CTH, E	q. (7)		None, Eq. (15)	None, Eq.	(9)	None, Eq. (12)	) $k_s, k_v, k_0$	$v_0, v_0, s_0, t_h$			
Ĺ	80	-ba	59	del	38	Model	Model	ACC			Spacing		Perception	Ve	ehicle	Acceleration	Calib	ration		
	81	MC	61	om	39	groups	ID	cont	roller		policy		delay (PD)	dy	namics (VD)	Constraints (AC)	param	neters		
	82	L-II	62	ised	40	S	19	Gipp	os, Eq. (4)-(3	5)	inherent		None, Eq. (15)	No	one, Eq. (9)	None, Eq. (12)	$\theta, v_0,$	$s_0, t_h, a_{max}, a_{min}$	, â <sub>min</sub>	
	83		63	-ba	41	del	20	Model	Model	ACC		Spacing		Percepti	on V	Vehicle	Acceleration	Calib	oration	



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#### Fig. 3. Overview of Formulas and calibration parameters of 90 models.

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This research was partially funded by the Italian program PON AIM - Attraction and International Mobility, Linea 1 (AIM1849341-2, CUP E61G18000540007).

All the data used are part of the JRC OpenACC database openly available online.

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(2)

(3)



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# Platoon trajectories in JRC OpenACC database

**Table 1.** Composition of platoons.
 Vehicle Platoons P3 P4 P5 P6 P7 position Audi A8 Audi A8 Audi A8 Leader Follower 1 Audi A6 Audi A6 Tesla Tesla Tesla



# Design of experiments

#### I. Optimization problem

$$\min_{\beta} f\left(Y^{obs}, Y^{sim}(\beta)\right),$$
$$Y^{sim}(\beta) = F(\beta),$$
$$IBa \leq \beta \leq UBa \ C(\beta) \leq 0$$

 $LD\beta \geq D \geq UD\beta, G(D) \geq 0,$  $\beta$  is the set of calibration parameters; F is the model; LB, UB, and G are constraints.

**II. Evaluation metric** 

f = NRMSE(Y),Goodness-of-fit (GoF) function: Measure of performance (*MoP*):  $Y \in [s, v, a],$ (18) $\operatorname{NRMSE}(s, v, a) = w_0 \operatorname{NRMSE}(s) + w_1 \operatorname{NRMSE}(v) + w_2 \operatorname{NRMSE}(a),$ NRMSE(Y) = RMSE(Y) /  $\sqrt{\frac{1}{N} \sum_{i=1}^{N} (Y_i^{obs})^2}$ ,  $RMSE(Y) = \sqrt{\frac{1}{N} \sum_{i=1}^{N} \left( Y_i^{sim} - Y_i^{obs} \right)^2},$ 

#### Table 2. Bounds of calibration parameters.

Parameter [unit]	Lower bound ( <i>LB</i> )	Upper bound ( <i>UB</i> )
$\delta$	0.1	10
$v_0$ [m/s]	30	35
<i>s</i> <sub>0</sub> [m]	1	5
<i>t<sub>h</sub></i> [s]	0.1	3
$a_{max}  [\text{m/s}^2]$	0.5	5
$a_{min}$ [m/s <sup>2</sup> ]	-5	-0.5
$\hat{a}_{min}$ [m/s <sup>2</sup> ]	-5	-0.5
$\theta$ [s]	0	3
$\tau_a$ [s]	0.3	0.8
$\tau_p$ [s]	0.1	0.8
$k_{s} [s^{-2}]$	0.01	5
$k_{v}  [s^{-1}]$	0.01	5
$k_0 [\text{s}^{-1}]$	0.01	5

## Conclusions

#### I. Contributions



- **Fig. 6.** Variability of normalized calibration errors ( $GoF_{i,ID}$ ) within (individual box plot) and among models
- Variance-based sensitivity analysis:  $S_{trajectories} = 0.819 > S_{models} = 0.062$ .
- Gipps-based models demonstrate the best performance in calibration experiments.
- Perception delay (PD) and linear vehicle dynamics (LVD) can improve model accuracy.
- Nonlinear vehicle dynamics (NLVD) can provide accuracy benefit to IDM- and Gipps-based models.



- > A comparison framework was proposed to assess CF/ACC models augmented at different levels of detail with vehicle dynamics, acceleration constraints, and perception delay. These physics extensions were essential aspects of human/automated driving behavior.
- > Two new spacing policies derived from microscopic traffic flow theory (TFT) were coupled with linear ACC controllers.
- Calibration experiments help to assess the contribution of each physics extension to the accuracy of the base model.

### **II.** Conclusions

- > Across all 90 model variants, Gipps-based models demonstrate the best performance in reproducing ACC driving trajectories.
- $\succ$  In terms of transferability of parameters and model robustness to vehicle collisions in validation experiments, IDM-based models outperform all other models, followed by Gipps-based ones.
- $\succ$  The objective (or GoF) function of NRMSE(s, v, a) can

Perception delay (PD) and linear vehicle dynamics (LVD) can

sensibly improve model robustness and transferability of

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1	4	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	73	76	79	82	85	88		
L																															
IDM-based models							Gin	ns-ba	ased	mode	els		L-CTH-based models						L-IDM-based models						L-Gipps-based models						
							ΟſΡ	P5 0.		1110 40												1110 4									
	$ID \in [1, 2,, 18]$						ID	∈[19.	, 20,	, 36	5]		ID∈[37, 38,, 54]						ID∈[55, 56,, 72]						$ID \in [73, 74,, 90]$						
								<b>-</b>	/ /	/																					

**Fig. 7.** Collision frequency (for each model variant) over 168 validation experiments.

- NRMSE(s, v, a) and Theil's U(s, v, a) lead to the least number of collisions in validation tests.
- IDM-based models outperform others regarding transferability of parameters and model robustness.

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largely improve model accuracy. > Nonlinear vehicle dynamics (NLVD) can provide accuracy benefit to IDM- and Gipps-based models.

calibrated parameters.

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